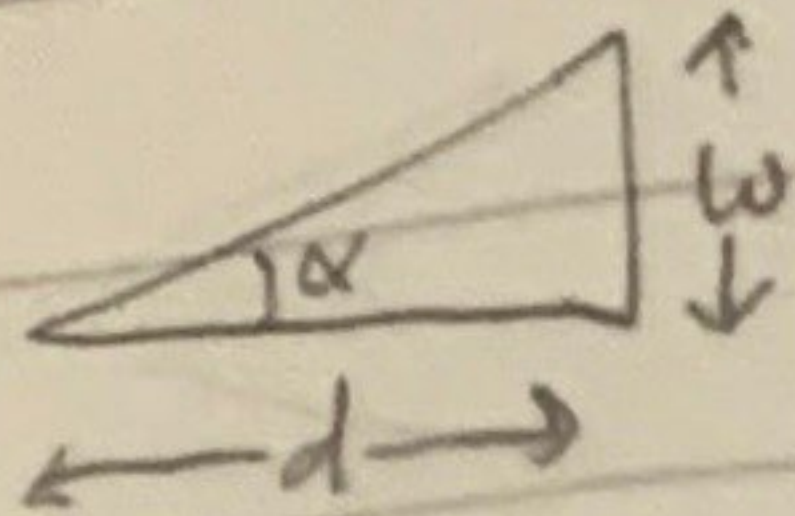
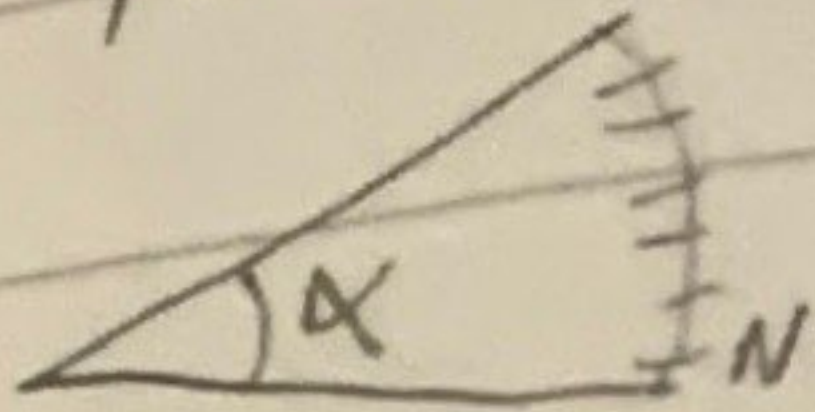


Optical Materials and Devices Problem Set

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14.1a) $\frac{1000 \text{ lumens}}{200 \text{ lumens/hr}} = 5W$ assuming an ideal source of white light

14.1b) spatial frequency: $\frac{N}{\alpha} = \frac{60 \text{ cycles}}{1^\circ} = 3438 \text{ cycles/rad}$
For $N=1$, $\alpha = 2.9 \cdot 10^{-4} \text{ rad}$



$$\frac{w}{d} = \tan \alpha \approx \alpha \rightarrow w = \alpha d$$

Plugging in: $w = (2.9 \cdot 10^{-4} \text{ rad})(0.5 \text{ m}) = 1.46 \cdot 10^{-4} \text{ m}$

$$\frac{1 \text{ dot}}{0.146 \text{ mm}} \cdot \frac{25.4 \text{ mm}}{1 \text{ in}} = 174 \text{ DPI}$$

14.2a) $U = \frac{8\pi h V^3}{c^3 (e^{h\nu/kT} - 1)}$ from Equation 13.5

To find the max: $\frac{\partial U}{\partial \nu} = 0 = \frac{8\pi h}{c^3} \frac{3\nu^2 (e^{h\nu/kT} - 1) - \nu^3 (\frac{h}{kT} e^{h\nu/kT})}{(e^{h\nu/kT} - 1)^2}$

$$0 = 3\nu^2 (e^{h\nu/kT} - 1) - \nu^3 \left(\frac{h}{kT} e^{h\nu/kT} \right)$$

$$0 = 3(e^{h\nu/kT} - 1) - \frac{h\nu}{kT} e^{h\nu/kT}$$

$$0 = 3(e^{h\nu/kT} - 1) - \frac{h\nu}{kT} e^{h\nu/kT}$$

$$3 = \left(\frac{h\nu}{kT} e^{h\nu/kT} \right) / (e^{h\nu/kT} - 1)$$

$$2.821 = \frac{h\nu}{kT} \rightarrow \nu = 2.821 \frac{kT}{h}$$

$$\lambda = \frac{c}{\nu} = \frac{hc}{2.821 kT}$$

$$36^\circ\text{C} + 273.15 = 309.15 \text{ K} \rightarrow \lambda = \frac{(6.626 \cdot 10^{-34} \text{ J}\cdot\text{s})(3 \cdot 10^8 \text{ m/s})}{2.821 (1.38 \cdot 10^{-23} \text{ J/K})(309.15 \text{ K})}$$

$$\rightarrow \lambda = 16.5 \text{ } \mu\text{m}$$

At $2.74 \text{ K} \rightarrow \lambda = 1.86 \text{ mm}$

14.2b) red appears at $\lambda = 700 \text{ nm}$

$$T = \frac{ch}{2.821 k \lambda} \approx 7300 \text{ K} = 7026.85^\circ \text{C}$$

14.2c) Stefan-Boltzmann Law (Equation 13.7): $R = 5.67 \cdot 10^{-8} T^4 \frac{\text{W}}{\text{m}^2}$

$$\text{Plug in } T = 309.15 \text{ K: } R = 5.67 \cdot 10^{-8} \cdot 309.15^4 = 517.9 \frac{\text{W}}{\text{m}^2}$$

$$14.3a) \begin{bmatrix} E_x' \\ E_y' \end{bmatrix} = e^{-i\sigma} \begin{bmatrix} e^{-i\delta} & 0 \\ 0 & e^{i\delta} \end{bmatrix} \begin{bmatrix} E_x \\ E_y \end{bmatrix} \text{ where } \sigma = (n_s + n_p) \frac{\omega d}{2c} \neq$$
$$\delta = (n_s - n_p) \frac{\omega d}{2c}$$

$$\text{For } 90^\circ \text{ turn: } \left. \begin{aligned} E_x' &= -E_y = e^{-i\sigma} e^{-i\delta} E_x \\ E_y' &= E_x = e^{-i\sigma} e^{i\delta} E_y \end{aligned} \right\} \begin{aligned} &\cdot |E_x| = |E_y| \\ &\therefore \text{(must start at } 45^\circ) \end{aligned}$$

$$\text{For } |E_x| = |E_y| = A: \begin{aligned} -1 &= e^{-i\sigma} e^{-i\delta} \\ 1 &= e^{-i\sigma} e^{i\delta} \end{aligned} \Rightarrow \begin{aligned} -1 &= e^{i2\delta} \\ 2\delta &= \pi(2a+1), a \in \mathbb{Z} \end{aligned}$$

From Question:

$$\text{thinnest } a = 0 \Rightarrow 2\delta = \pi$$

$$\delta = \frac{\pi}{2} = (n_s - n_p) \frac{\omega d}{2c}$$

$$\omega = \frac{2\pi c}{\lambda} \Rightarrow \frac{\pi}{2} = (n_s - n_p) \frac{2\pi c d}{2c \lambda}$$

$$\Rightarrow \frac{1}{2} = (n_s - n_p) \frac{d}{\lambda}$$

$$d = \frac{\lambda}{2(n_s - n_p)}$$

$$\text{For calcite: } n_s = 1.658, n_p = 1.486$$

$$\text{Plugging in: } d = \frac{600 \text{ nm}}{2(1.658 - 1.486)} = 1.744 \mu\text{m}$$

$\hookrightarrow$ this ends up being a half wave plate
(at higher multiples)

14.3b) Goal to design a quarter wave plate

14.3c) Now we want to rotate them,

I had trouble
solving these properly.

$$14.4) \gamma_x - \gamma_y = \pi = \frac{1}{c} \omega n_o^3 r_{63} V \quad (\text{Equation 13.30})$$

Plug in $\omega = \frac{2\pi c}{\lambda} \rightarrow \pi = \frac{2\pi c}{\lambda} n_o^3 r_{63} V$

$$V = \frac{\lambda}{2 n_o^3 r_{63}} = \frac{700 \text{ nm}}{2 (1.51)^3 (10.6 \cdot 10^{-3} \text{ m/V})}$$

$$V = 9.59 \text{ kV} \quad \text{There are kW op-amps available now.}$$

14.5a) Equation 13.34 (Bragg diffraction condition):

$$2 \lambda_{\text{photon}} \sin \theta = \frac{\lambda_{\text{photon}}}{n} \quad \text{where } \lambda_{\text{photon}} = \frac{v}{v_s}$$

$$\theta = \arcsin \left(\frac{\lambda_{\text{photon}} v_s}{2 \lambda} \right)$$

$$= \arcsin \left(\frac{700 \text{ nm} (100 \cdot 10^6 \text{ Hz})}{2 (1.51) (2.25)} \right)$$

$$= \arcsin (2.1 \cdot 10^{-3}) = 0.12^\circ$$

$$14.5b) \frac{I_{\text{diff}}}{I_{\text{in}}} = \sin^2 \left(\frac{\pi e \sqrt{\mu} I_a}{\lambda \sqrt{2}} \right) \quad (\text{Equation 13.35})$$

$$I_a = \frac{1 \text{ W}}{(1 \text{ mm})^2} = \frac{1 \mu \text{ W}}{\text{m}^2}$$

$$M = \frac{h^2 c^2 p^2}{\rho v_s^3} \xrightarrow{\text{Plug in}} \frac{(2.25)^6 (0.15)^2}{(4700 \frac{\text{kg}}{\text{m}^3}) (7.4 \cdot 10^3 \frac{\text{m}}{\text{s}})^3}$$

$$= 1.53 \cdot 10^{-15} \frac{\text{m}^2}{\text{W}}$$

$$\Rightarrow \frac{I_{\text{diff}}}{I_{\text{in}}} = \sin^2 \left(\frac{\pi (10^{-3} \text{ m}) \sqrt{1.533 \cdot 10^{-15} (1 \cdot 10^6)}}{100 \cdot 10^{-9} \text{ m} \sqrt{2}} \right)$$

$$= 0.015 \quad (\text{AO modulators are fast w/ no moving parts})$$

$\rightarrow$ faster than typical tiltable mirrors but not efficient at getting all the light through

$$14.5c) N = \frac{\Delta V_s D}{v_s} \rightarrow \Delta V_s = \frac{N v_s}{D} = \frac{(1000) (7.4 \cdot 10^3 \frac{\text{m}}{\text{s}})}{10^{-2} \text{ m}}$$

$$= 740 \text{ MHz}$$

acousto-optic modulators