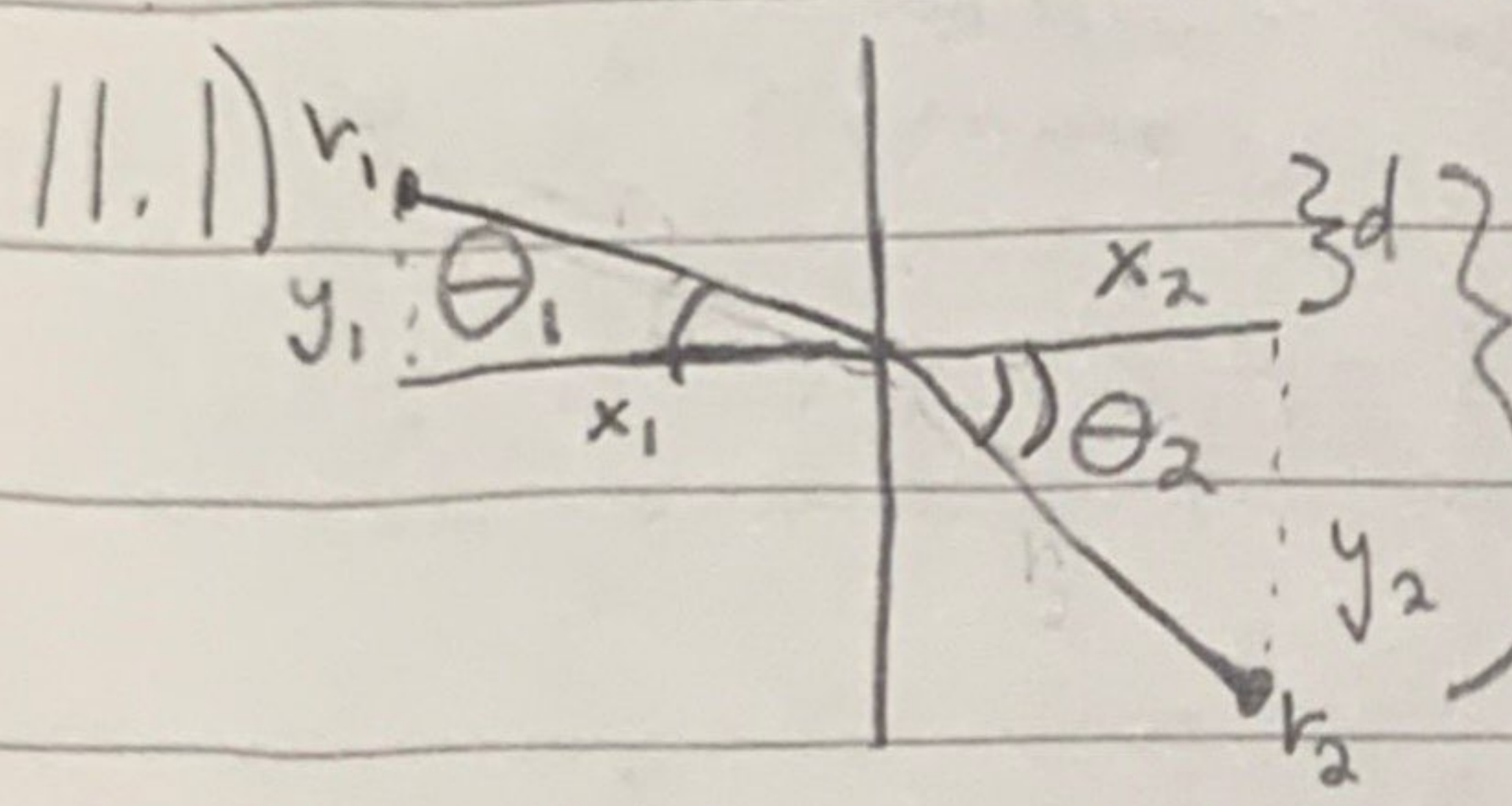


Optics Problem Set

Sara V. Fernandez
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11.1)  The total time needed to travel from r_1 to r_2 :

$$t = \frac{\sqrt{x_1^2 + y_1^2}}{v_1} + \frac{\sqrt{x_2^2 + y_2^2}}{v_2}$$

where v_1 & v_2 are the speeds of light in the materials.

Redefining t in terms of d since t is minimized by Fermat's principle:

$$t = \frac{\sqrt{x_1^2 + d^2}}{v_1} + \frac{\sqrt{x_2^2 + (h-d)^2}}{v_2}$$

Solving for the minimum travel time (where $\frac{dt}{dx} = 0$):

$$0 = \frac{dt}{dx} = \frac{1}{2} \frac{(x_1^2 + d^2)^{-1/2}}{v_1} \cdot 2d + \frac{1}{2} \frac{(x_2^2 + (h-d)^2)^{-1/2}}{v_2} \cdot 2(h-d) \cdot (-1)$$

$$0 = \frac{d}{v_1 \sqrt{x_1^2 + d^2}} - \frac{h-d}{v_2 \sqrt{x_2^2 + (h-d)^2}}$$

$$0 = \frac{\sin \theta_1}{v_1} - \frac{\sin \theta_2}{v_2} \rightarrow \frac{v_1}{v_2} = \frac{\sin \theta_1}{\sin \theta_2}$$

Plug in $v_1 = \frac{c}{n_1}$ & $v_2 = \frac{c}{n_2}$ (speed in terms of refractive index):

$$\frac{c}{n_1} \cdot \frac{n_2}{c} = \frac{\sin \theta_1}{\sin \theta_2} \rightarrow n_1 \sin \theta_1 = n_2 \sin \theta_2$$

Snell's Law is confirmed to be $n_1 \sin \theta_1 = n_2 \sin \theta_2$

11.2) Fresnel's Equations (10.20 & 10.24):

s-polarized & transmitted $E_{\perp} = \frac{2 \sin \theta_2 \cos \theta_0}{\sin(\theta_2 + \theta_0)} E_0$ & p-polarized & transmitted $E_{\parallel} = \frac{2 \cos \theta_0 \sin \theta_2}{\sin(\theta_0 + \theta_2) \cos(\theta_0 - \theta_2)} E_0$

s-polarized & reflected $E_{\perp} = \frac{\sin(\theta_2 - \theta_0)}{\sin(\theta_2 + \theta_0)} E_0$ (no reflection if materials are the same or

when TX & RX are $\perp \rightarrow \theta_0 = \theta_2$ or $\theta_0 + \theta_2 = \frac{\pi}{2}$)

p-polarized & reflected $E_{\parallel} = \frac{\tan(\theta_0 - \theta_2)}{\tan(\theta_0 + \theta_2)} E_0$

Poynting vector: $S = \vec{H} \times \vec{E}$ needs a k too,
(but cancels out anyway)

TEM wave: $S = |\vec{H}| |\vec{E}| \hat{k}$ & $|\vec{H}| = \frac{1}{\omega \mu_0} \hat{k} \times \vec{E} = \frac{1}{\mu_m} E$

$\therefore S = \frac{1}{\omega \mu_0} \cdot E^2 \hat{k}$

$$\langle S \rangle_{in} = \frac{1}{\omega \mu_0} \langle E^2 e^{-2i(\vec{k} \cdot \vec{r} + \omega t)} \rangle = \frac{1}{2\omega \mu_0} E_0^2$$

$$\begin{aligned} \langle S \rangle_{reflected} &= \frac{1}{\omega \mu_0} (E_{\perp}^{R_2} + E_{\parallel}^{R_2}) \quad (\text{avg of two polarizations}) \\ &= \frac{1}{\omega \mu_0} E_0^2 \left(\frac{\sin^2(\theta_2 - \theta_0)}{\sin^2(\theta_2 + \theta_0)} + \frac{\tan^2(\theta_0 - \theta_2)}{\tan^2(\theta_0 + \theta_2)} \right) \end{aligned}$$

$$\begin{aligned} \langle S \rangle_{transmitted} &= \frac{1}{\omega \mu_0} (E_{\perp}^{T_2} + E_{\parallel}^{T_2}) \\ &= \frac{1}{\omega \mu_0} E_0^2 \left(\frac{4 \sin^2 \theta_2 \cos^2 \theta_0}{\sin^2(\theta_2 + \theta_0)} + \frac{4 \sin^2 \theta_2 \cos^2 \theta_0}{\sin^2(\theta_2 + \theta_0) \cos^2(\theta_2 - \theta_0)} \right) \end{aligned}$$

$$\therefore R = \underbrace{\left(\frac{\sin(\theta_2 - \theta_0)}{\sin(\theta_2 + \theta_0)} \right)^2}_{(s\text{-polarized})} + \underbrace{\left(\frac{\tan(\theta_2 - \theta_0)}{\tan(\theta_2 + \theta_0)} \right)^2}_{(p\text{-polarized})}$$

$$T = \underbrace{\left(\frac{2 \sin \theta_2 \cos \theta_0}{\sin(\theta_2 + \theta_0)} \right)^2}_{(s\text{-polarized})} + \underbrace{\left(\frac{2 \sin \theta_2 \cos \theta_0}{\sin(\theta_2 + \theta_0) \cos(\theta_2 - \theta_0)} \right)^2}_{(p\text{-polarized})}$$

b) At normal incidence: $R = \left(\frac{n_1 - n_2}{n_1 + n_2} \right)^2 = \left(\frac{1.5 - 1}{1.5 + 1} \right)^2 = 0.04$

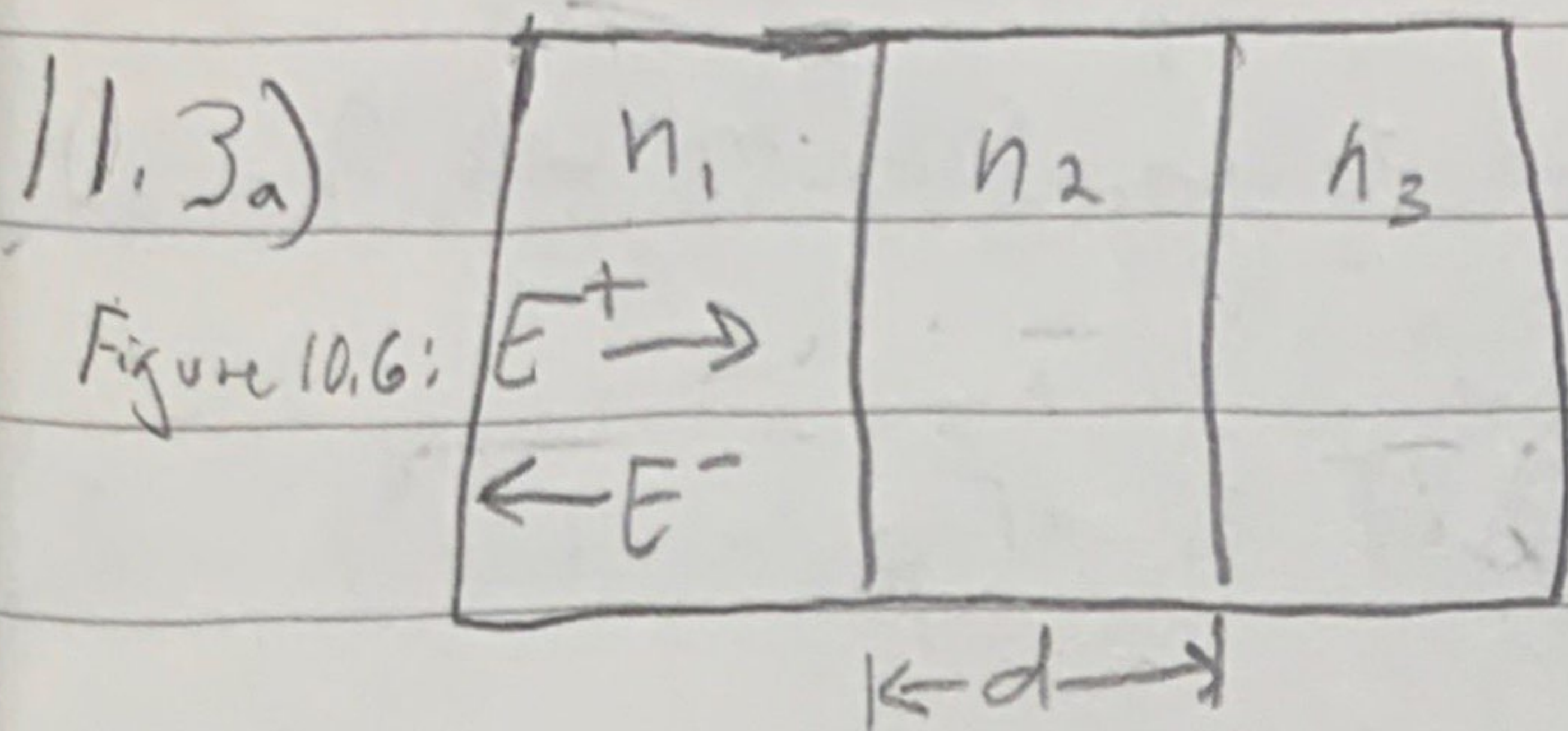
c) $\theta_c = \tan^{-1} \left(\frac{n_2}{n_1} \right)$

For glass-air interface, $n_1 = 1$ & $n_2 = 1.5 \therefore \theta_c = 56.3^\circ$

For air-glass interface, $n_1 = 1.5$ & $n_2 = 1 \therefore \theta_c = 33.7^\circ$

d) critical angle $\theta_c = \sin^{-1} \left(\frac{n_1}{n_2} \right) \rightarrow$ For glass-air interface, $\theta_c = 41.8^\circ$

11.3a)



$$R_{ij} = \frac{n_i - n_j}{n_i + n_j} \quad (\text{reflection})$$

$$T_{ij} = \frac{2n_i}{n_i + n_j} \quad (\text{transmission})$$

$$\varphi = e^{ik_2 d} \quad (\text{phase change})$$

Total reflection intensity:

equivalently

$$E_R = E_0 (R_{12} + T_{12} R_{23} e^{ik_2 2d} T_{21} + T_{12} R_{23} e^{ik_2 2d} R_{21} R_{23} e^{ik_2 2d} R_{21} R_{23} e^{ik_2 2d} T_{21} + \dots)$$

$$E_R = E_0 (R_{12} + T_{12} R_{23} e^{ik_2 2d} T_{21} \sum_{n=0}^{\infty} (R_{21} R_{23} e^{ik_2 2d})^n)$$

Simplify using $\sum_{n=0}^{\infty} x^n = \frac{1}{1-x}$:

$$E_R = E_0 \left(R_{12} + \frac{T_{12} R_{23} e^{ik_2 2d} T_{21}}{1 - R_{21} R_{23} e^{ik_2 2d}} \right) \text{ where } R_{12} = -R_{21}$$

$$E_R = E_0 \left(\frac{R_{12} + R_{12}^2 R_{23} e^{ik_2 2d} + T_{12} R_{23} e^{ik_2 2d} T_{21}}{1 + R_{12} R_{23} e^{ik_2 2d}} \right)$$

$$= E_0 \left(\frac{R_{12} + R_{23} e^{ik_2 2d} (R_{12}^2 + T_{12} T_{21})}{1 + R_{12} R_{23} e^{ik_2 2d}} \right)$$

Simplify in parts: $R_{12}^2 + T_{12} T_{21} = \frac{(n_1 - n_2)^2}{n_1 + n_2} + \frac{4n_1 n_2}{(n_1 + n_2)^2}$

$$\rightarrow = \frac{n_1^2 - 2n_1 n_2 + n_2^2 + 4n_1 n_2}{n_1^2 + 2n_1 n_2 + n_2^2} = 1$$

$$E_R = E_0 \left(\frac{R_{12} + R_{23} e^{ik_2 2d}}{1 + R_{12} R_{23} e^{ik_2 2d}} \right)$$

Plug in: $R = \frac{|E_R|^2}{|E_0|^2} = \left(\frac{R_{12} + R_{23} e^{ik_2 2d}}{1 + R_{12} R_{23} e^{ik_2 2d}} \right)^2$

11.36) The reflection disappears during destructive interference:

$$\phi = \frac{4\pi n_2 d}{\lambda} = (2m+1)\pi \quad (\text{phase shift})$$

$$\therefore d = \frac{(2m+1)\lambda}{4n_2}$$

For maximum thickness condition, $m=0$:

$$\therefore d = \frac{\lambda}{4n_2}$$

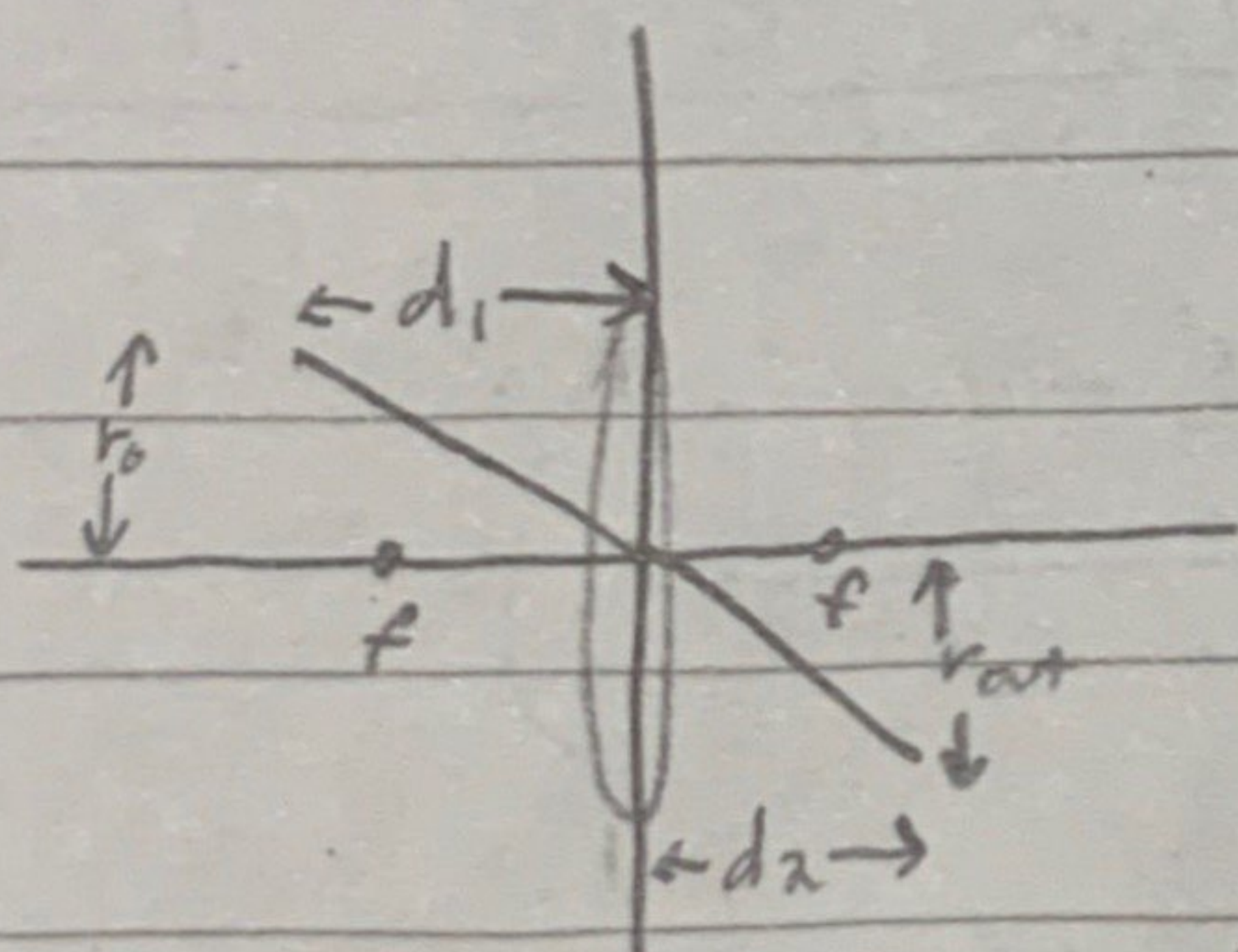
$$\text{Also, } 0 = \frac{R_{12} + R_{23}}{1 + R_{12}R_{23}} \rightarrow R_{12} = R_{23}$$

$$\frac{n_1 - n_2}{n_1 + n_2} = \frac{n_2 - n_3}{n_2 + n_3}$$

$$\text{Solve: } n_1 n_2 + n_1 n_3 - n_2^2 - n_2 n_3 = n_1 n_2 - n_1 n_3 + n_2^2 - n_2 n_3$$

$$\therefore n_2 = \sqrt{n_1 n_3}$$

11.4)



(using ray matrices)

$$M_{\text{tot}} = M_{\text{prop}_2} \cdot M_{\text{lens}} \cdot M_{\text{prop}_1}$$

$$\begin{bmatrix} r_{\text{out}} \\ r'_{\text{out}} \end{bmatrix} = \begin{bmatrix} 1 & d_2 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ -1/f & 1 \end{bmatrix} \begin{bmatrix} 1 & d_1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} r_o \\ r'_o \end{bmatrix}$$

$$= \begin{bmatrix} 1 & d_2 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & d_1 \\ -1/f & 1 - d_1/f \end{bmatrix} \begin{bmatrix} r_o \\ r'_o \end{bmatrix}$$

$$\begin{bmatrix} r_{\text{out}} \\ r'_{\text{out}} \end{bmatrix} = \begin{bmatrix} 1 - d_2/f & d_1 + d_2(1 - d_1/f) \\ -1/f & -d_1/f \end{bmatrix} \begin{bmatrix} r_o \\ r'_o \end{bmatrix}$$

For all rays to converge on the image plane, r'_o must = 0 (This makes it independent of angle)

$$\therefore d_1 + d_2(1 - d_1/f) = 0$$

$$\text{Solve for } d_2: d_2 = \frac{d_1 f}{d_1 - f} \xrightarrow{\text{thin lens eqn}} \frac{1}{d_1} + \frac{1}{d_2} = \frac{1}{f} \quad (\text{Eqn. 10.35})$$

$\therefore$ All rays will meet at the image plane at a distance d_2 from the thin lens.

$$\text{Looking at magnification: } M = \frac{r'_o}{r_o} = A = 1 - d_o/f \quad (\text{magnification})$$

11.5a) divergence angle $\theta = \frac{\lambda}{\pi n w}$ where $\lambda = 790 \text{ nm}$ & $D = 1 \text{ mm}$

$$\theta = \frac{790 \cdot 10^{-9}}{\pi \cdot 1 \cdot 10^{-6}}$$

Beam divergence angle is $\theta = 0.251 \text{ rad} \rightarrow \theta = 14.4^\circ$

11.5b) $\lambda_{\text{new}} = \lambda \cdot \frac{D_{\text{new}}}{D}$ (also $\lambda = \theta \cdot \pi n w = 0.251 \cdot \pi \cdot 1 \cdot 10^{-6}$)

$$\lambda_{\text{new}} = 790 \cdot \frac{1 \times 10^{-7}}{1 \cdot 10^{-6}} \rightarrow \lambda_{\text{new}} = 79 \text{ nm}$$

11.5c) $\theta = \frac{600 \text{ nm}}{\pi \cdot 1 \cdot 10 \text{ cm}} = 1.9 \cdot 10^{-5} \text{ rad}$ where $10 \text{ cm} = \text{license plate size}$

Knowns: $\lambda = 600 \text{ nm}$, $h = 0.1 \text{ m}$, $L = 200 \text{ km} = 2 \cdot 10^5 \text{ m}$

$$r = h \tan \theta \approx h \theta$$

$$\frac{h}{L} > \frac{1.22 \lambda}{D}$$

$$r = (200 \text{ km}) (1.9 \cdot 10^{-5}) = 3.8 \text{ m}$$

Plug in and solve for D : $D > 1.46 \text{ cm}$ $\rightarrow 2 \cdot 10^3 \text{ km} \cdot 1.9 \cdot 10^{-5} \text{ rad} = 3.8 \text{ m}$

11.6) Periodically forced Lorentz model to find dielectric constant as a function of f

$$m \ddot{x} + m \gamma \dot{x} + m \omega_0^2 x = -e E_0 e^{-i \omega t} \quad \text{where } E_0 e^{-i \omega t} = E(t)$$

Assuming a steady-state response as in $x = x_0 e^{-i \omega t}$, solve for x_0 :

$$x_0 = \frac{-e E_0}{m(\omega_0^2 - \omega^2 - i \gamma \omega)}$$

Solve for induced polarization: $P = N p$ (dipole moment / unit volume)

Since $p = -e x \therefore P = -N e x$

Substitute x_0 into P :

$$P = -Nex = Ne^2 \left(\frac{E_0}{m(\omega_0^2 - \omega^2 - i\gamma\omega)} \right) \text{ where } N \text{ is \# oscillators / unit volume}$$

Use the expression for the dielectric constant:

$$D = \epsilon_0 E + P$$

$$\epsilon(\omega) = \epsilon_0 \left(1 + \frac{Ne^2}{\epsilon_0 m} \frac{1}{\omega_0^2 - \omega^2 - i\gamma\omega} \right)$$

plasma frequency: $\omega_p^2 = \frac{Ne^2}{\epsilon_0 m}$

$$\epsilon(\omega) = \epsilon_0 \left(1 + \frac{\omega_p^2}{\omega_0^2 - \omega^2 - i\gamma\omega} \right)$$

wherein $\text{Re}(\omega)$ is dispersion & $\text{Im}(\omega)$ is absorption loss

This is plotted as Figure 10.5 Anomalous dispersion.

