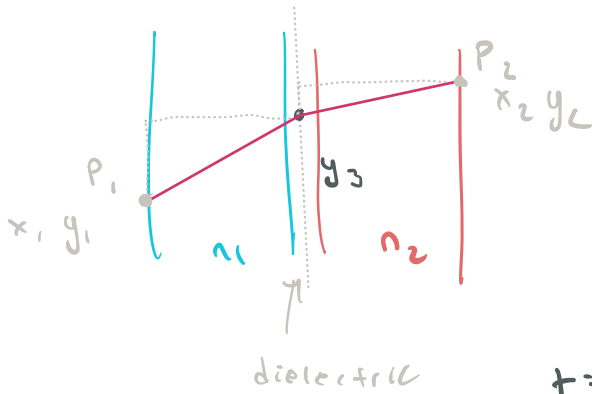


9.1) FERMAT'S PRINCIPLE  $\rightarrow$  SNELL'S LAW



time to go from  $P_1$  to  $P_2$

take derivative  $\rightarrow$   
 + set = 0 to find min

$$t = \frac{n_1}{c} \sqrt{x_1^2 + (y_1 - y_3)^2}$$

$$+ \frac{n_2}{c} \sqrt{x_2^2 + (y_2 - y_3)^2}$$

$$0 = \frac{dt}{dy} = \frac{-n_1(y_1 - y_3)}{c \sqrt{x_1^2 + (y_1 - y_3)^2}} + \frac{-n_2(y_2 - y_3)}{c \sqrt{x_2^2 + (y_2 - y_3)^2}}$$

$$0 = -\frac{n_1 \sin \theta_1}{c} + \frac{n_2 \sin \theta_2}{c}$$

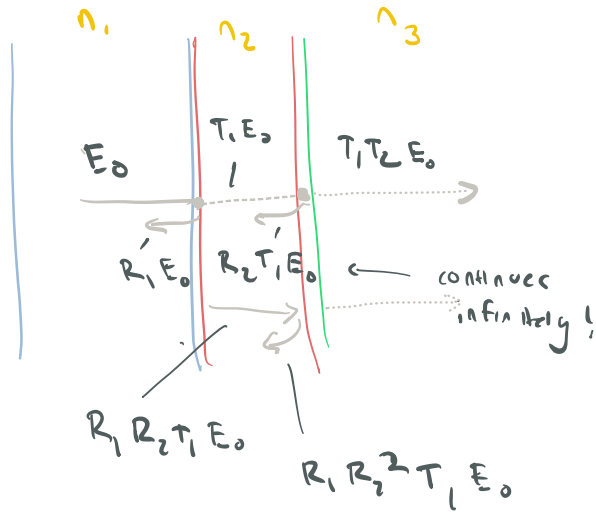
$$n_1 \sin \theta_1 = n_2 \sin \theta_2$$

$$\text{or } \frac{n_1}{n_2} = \frac{\sin \theta_2}{\sin \theta_1}$$

9.2)

9.3)

a)



single interface  
reflectivity

$R_1$   $R_2$

Transmissivity

$T_1$   $T_2$

can  
be  
derived  
from  
 $n_1$  &  $n_2$

So we have:

$$R_{\text{total}} = E_0 \left( R_1 + R_2 T_1^2 + R_2^2 T_1^2 R_1 \dots \right)$$

$T_1^2$  will remain constant after here

but we keep adding  $R_1$ 's &  $R_2$ 's

$$R_{\text{total}} = R_1 E_0 + \sum_{n=0}^{\infty} E_0 T_1^2 R_2^{n+1} R_1^n$$

Note that we can relate  $n$  to  $T$  &  $R$   
by:

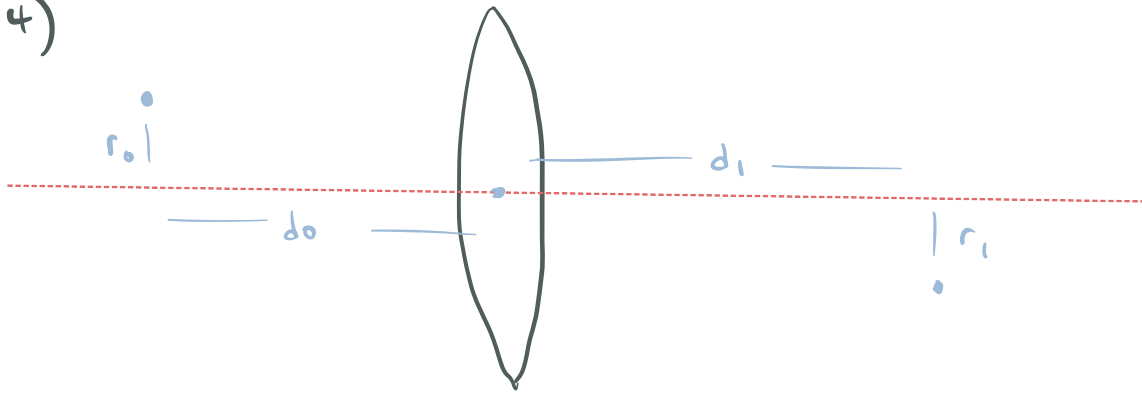
$$R = \frac{n_1 \cos \theta - n_2 \cos \theta}{n_1 \cos \theta + n_2 \cos \theta} \quad (\text{all } \theta)$$

$$= \frac{n_1 - n_2}{n_1 + n_2}$$

$$T = \frac{2n_1}{n_1 + n_2}$$

b) to get  $R = 0$

9.4)



9.5) for  $\lambda = 790 \text{ nm}$

a) beam divergence angle for d.f. grating of  $1 \mu\text{m}$

since d.f. limited:

eq.  
(9.52)  $\theta = \frac{\lambda}{\pi n w}$

where  $n = \text{index of refraction}$   
 $w = \text{waist radius}$   
(min beam diameter)

$$\theta = \frac{790 \text{ e}^{-9}}{\pi (1) (1 \text{ e}^{-6})}$$

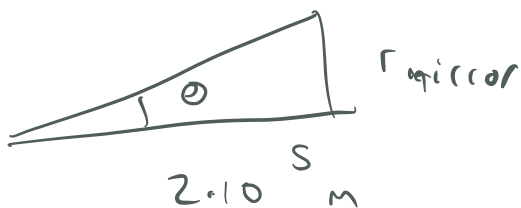
we know  $w$  must be in the order of the grating, so:

$$< 0.251 \text{ rads}$$

b) same but we would need  $10 \times$  smaller wavelength

c) assuming  $w = 1 \mu\text{m} = 1 \text{ e}^{-3}$

$$\theta = \frac{600 \text{ e}^{-9}}{\pi (1) (1 \text{ e}^{-3})} = 190 \text{ e}^{-6}$$



$$\tan \theta = \frac{r_{\text{mirror}}}{2.10^5 \text{ m}}$$

$$= 38 \text{ meters!}$$